Chandra Sekhar G and Ming-Jer Lee. /Asian Journal of Research in Chemistry and Pharmaceutical Sciences. 7(1), 2019, 114-121. Research Article ISSN: 2349 – 7106



# Asian Journal of Research in Chemistry and

**Pharmaceutical Sciences** 

Journal home page: www.ajrcps.com



## PHASE EQUILIBRIA FOR BINARY MIXTURES OF NONANE WITH OCTANE AND OCTANE WITH ORTHOXYLENE, METAXYLENE AT 101.3 kPa

## G. Chandra Sekhar\*1 and Ming-Jer Lee<sup>2</sup>

<sup>1\*</sup>Department of Chemistry, Government Degree and PG College, Puttur, Chittoor, 517 583, (Affiliated to S V University, Tirupati), Andhra Pradesh, India.
<sup>2</sup>Department of Chemical Engineering, National Technology, 42 Keelung, 43 Keelung, 44 Keelung, 45 Keelun

<sup>2</sup>Department of Chemical Engineering, National Taiwan University of Science and Technology, 43 Keelung Road, Section 4, Taipei 106-07, Taiwan.

## ABSTRACT

Isobaric vapour-liquid equilibrium boiling temperature measurements have been determined at 101.3 kPa as function of composition for the binary mixtures of nonane with octane and octane with orthoxylene and metaxylene by using a recirculation type apparatus. The experimental temperature, vapour and liquid composition (T-x-y) results were correlated with the NRTL and UNIQUAC models. All systems studied here behave like non-ideal solutions.

## **KEYWORDS**

Nonane, Octane, Orthoxylene, Metaxylene, Isobaric, Vapour liquid equilibrium and Binary.

## Author for Correspondence:

Chandra Sekhar G,

Department of Chemistry,

Government Degree College,

Puttur, Chittoor, 517 583, Andhra Pradesh, India.

Email: csgandii3@gmail.com

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## **INTRODUCTON**

Experimental data of excess thermodynamic properties of liquids and liquid mixtures are of great fundamental and practical importance. These properties allow one to draw information on the structure and interactions of mixed solvents. The knowledge of phase equilibrium properties of liquid mixtures are fascinating and of great fundamental, practical importance, and industrial points of view. An accurate and complete knowledge of VLE data on the mixtures under consideration is necessary for the design of distillation equipment. In general, alkanes show a relatively low reactivity, because their C bonds are relatively stable and cannot be easily broken. Unlike most other organic January – March 114

compounds, they possess no functional groups. Oil is a mixture of liquid alkanes and other hydrocarbons. The most important commercial sources for alkanes are natural gas and oil<sup>1</sup>. Our current project is devoted to the systematic study of liquid systems containing aliphatic and aromatic hydrocarbons with respect to their environmental importance. From a practical point of view, the data are useful for the design of mixing, storage, and process equipment. This behaviour can be attributed mainly to the specific interactions between unlike molecules of the systems. Our new project is devoted to the systematic study of liquid systems modeling liquid engine fuels.

Nonane and octane are good solvents and non-polar, water in soluable volatile liquids. Nonane and are used as fuels in internal combustion engines, as they vaporize easily on entry into the combustion chamber without forming droplets, which would impair the uniformity of the combustion. The separation of aromatic hydrocarbons (benzene, toluene and xylenes) from aliphatic hydrocarbons (octane and nonane) mixtures is challenging scientists from many years. The aromatic liquids used in this study are very important in petrochemical industries, and several studies on their physical properties at different temperatures and  $pressures^{2-5}$  have been published.

Xylenes are refers to a mixture of three aromatic hydrocarbon isomers. essentially benzene derivatives, which are used as good solvent in the printing, rubber and leather industries. The xylenes are clear, colourless and sweet-smelling liquids that are very flammable. The xylenes are usually refined from crude oil in a process called alkylation. Like other solvents, xylenes are also used as an inhalant drug for its intoxicating properties. In biochemistry, xylene is also used for making slides of specimens hydrophobic in preparation for coverslip mounting. Xylenes are a starting material for the production of other chemicals. For instance chlorination of both methyl groups gives three isomeric xylene dichlorides or 1, 2-bis (chloromethyl) benzenes. With oxidizing agents, such as KMnO<sub>4</sub>, the methyl group can be oxidized to a carboxylic acid. By oxidizing both methyl groups, o-xylene forms Available online: www.uptodateresearchpublication.com

phthalic acid. o-Xylene is largely used in the production of phthalic anhydride. The major chemical use of metaxylene is in the manufacture of isophthalicacid, which is used as a copolymer to alter the properties of polyethylene terephthalate (PET) making. The PET more suitable for the manufacture of soft drinks bottles.

Vapour-liquid equilibria data are required for design and operation of distillation equipment and for determining the optimal values of parameters in the thermodynamic models. As part of our research program to explore the VLE of various molecular liquids<sup>6-11</sup>, we report here the VLE measurements for the binary systems of nonane with octane and octane with orthoxylene and metaxylene at101.3 kPa with a circulating type apparatus. Our literature survey reveals that there has been no effort to collect the VLE for the mixtures of nonane with octane with orthoxylene octane and and metaxylene. The equations of the  $NRTL^{12}$  and the UNIQUAC<sup>13</sup> were used to correlate the experimental VLE data of the binary systems.

## **EXPERIMENTAL**

## Materials

In the present study, all the chemicals used were of analytical grade and purchased from commercial sources. The purities of used chemicals were given here in the form of percentage, Nonane (99.98%, Aldrich, USA), octane (99.94%, Aldrich, USA), orthoxylene (99.97%, Alfa Aeser, USA) and metaxylene (99.99%, Acros, USA). The purity of with each chemical was checked gas chromatography failed to show any significant impurities. The purity of the chemicals was assessed by comparing their measured densities  $(\rho)$ , with Anton Paar (DMA 4500) digital vibrating-tube densimeter, which were in good agreement with the literature values<sup>14-18</sup>, as can be seen in Table No.1.

## **VLE measurements**

A recirculation-type phase equilibrium apparatus (NGW Co., Germany) was used in this study to measure the isobaric VLE data. The schematic diagram and the detailed operation procedure have been given by Shiah et al.<sup>19</sup>. The major parts of the equilibrium apparatus was divided into four major January – March

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parts, a liquid-phase chamber, a condenser, a vaporphase cell and two coil heaters. A silicon oil jacket surrounded the outer spaces of the liquid-phase chamber and the vapor-phase cell. To maintain isothermal condition inside the jacket, the coil heaters were controlled by a PID controller. The top of the equilibrium still was connected to a burette and an adjustable water reservoir to manipulate the total pressure of the system at 101.3 0.2 kPa. The boiling temperature was measured by a series of precision thermometers (models N6000-N6020, stability = 0.1 K, Amarell Electronic Co., Germany). The atmospheric pressure was measured by a Fortin mercury barometer (model 453, stability = 0.1 kPa, Princo Instruments, USA).

The phase compositions were analyzed by gas chromatography (GC) with a thermal conductivity detector. GC model 8700 (China Chromatography, Taiwan) were employed to the isobaric VLE measurements. High-purity Helium (99.99 %) was used as a carrier gas in GC in the present investigation.

The boiling points of mixtures of nonane with hexane, heptane, octane and octane with orthoxylene and metaxylene were measured at 101.3 kPa over the entire range of composition.

## **RESULTS AND DISCUSSION**

In the present study, the isobaric VLE results (T, x and y) were correlated with the -  $\gamma$  method by using one of the activity coefficient models (the  $NRTL^{12}$ , the UNIQUAC  $^{13}$ ) and assuming that the vapour phase was that of ideal gas mixtures. In the VLE data reduction, the component's fugacity in the vapor phase was calculated from the two-term virial equation of state. The NRTL and the UNIQUAC models were adopted, respectively, to represent the non-ideality of the constituent compounds in the liquid phase. The binary interaction parameters of the solution models (ii value of the NRTL was fixed to be 0.3 through the VLE data reduction) were determined on the basis of the maximum likelihood principle by minimization of the following objective function,  $\Pi_1$ :

$$\pi_{1} = \sum_{k=1}^{n_{p}} \left\{ \left[ \frac{\left[ I_{k}^{calc} - I_{k}^{exp} \right]}{\sigma_{p}} \right]^{2} + \left[ \frac{\left[ I_{k}^{calc} - I_{k}^{exp} \right]}{\sigma_{T}} \right]^{2} + \left[ \frac{\left[ x_{1,k}^{calc} - x_{1,k}^{exp} \right]}{\sigma_{x_{i}}} \right]^{2} + \left[ \frac{\left[ x_{1,k}^{calc} - x_{1,k}^{exp} \right]}{\sigma_{y_{i}}} \right]^{2} \right\}$$
(1)

where  $T^{exp}_k$  and  $T^{calc}_k$  are the experimental and the calculated boiling point temperatures, respectively, and summation is performed over all experimental points.

The standard deviations of the measured variables are 0.1 kPa for pressure, 0.1 K for temperature, 0.002 for liquid composition, and 0.005 for vapor composition. The Antoine constants for vapour pressures of the pure components were taken from the literature  $^{14,20,21}$  and are presented in Table No.2, while the optimized values of the parameters, g12, g21 and of the NRTL, and u12 and u21 of the UNIQUAC are collected in Table No.3. The boiling point temperature versus mole fraction of liquid phase and vapour phase curves are presented in Figure No.1-3. Each binary system has passed the thermodynamic consistency test of Herington<sup>22</sup>. The smooth curves in the graph are the calculated values from the UNIQUAC model for both the liquid and vapour phases. Such a study on model calculations in addition to presentation of experimental data on binary mixtures are useful to understand the mixing behaviour of liquids in terms of molecular interactions and orientation order-disorder effects. For sake of clarity, we did not show here the other two models, since three models are merging. The close observation of Figure No.1-3 reveals that the curves of three models are overlapping on one another. All these three models with the tabulated parameters represent good agreement with the VLE properties of nonane with octane and octane with orthoxylene and metaxylene at 101.3 kPa. The results reveal that all the systems studied exhibit non-ideal behaviour. In the studied systems especially octane with orthoxylene and metaxylene so the differences in T, x and y can be attributed primarily to the differences in the aliphatic-aromatic interaction energy. For the systems nonane with octane in which the behaviour of vapour and liquid compositions are non ideal. The deviations from ideal behaviour of the systems studied can be

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discussed in terms of molecular interactions as follows. On the contrary, in the systems (octane + orthoxylene and metaxylene) we should consider not only the packing effects but also the dominating specific n- interactions. If we observe Figure No.1 closely the gap between liquid phase and vapour phase is wider than that of gap between liquid phase and vapour phase of Figure No.2 and Figure No.3 of nonane with heptane and octane. We can also observe in Figure No.2 the gap between liquid phase and vapour phase is lesser than that of nonane with hexane and wider than that of nonane with octane (Figure No.3). Finally we conclude that the carbon number in alkanes increases non ideal nature decreases. Whereas in the cases of octane with orthoxylene and metaxylene (Figure No.4 and 5) their behaviour is nonideal but tendency is similar because orthoxylene and metaxylenes are isomers. As we shown in Figure No.1-3, nonane with octane and octane with orthoxylene and metaxylene systems show relatively larger deviations from Raoults's law. All systems does not show azeotropic behaviour.

S.No	Compound	ρ /(g-c	m <sup>-3</sup> )	<i>T</i> /K		
	Compound	This work	Literature	This work	Literature	
1	Nonane	0.71374	0.71375 <sup>a</sup>	423.55	424.00 <sup>d</sup>	
2	Octane	0.69863	0.69862 <sup>a</sup>	398.33	398.82 <sup>a</sup>	
3	Orthoxylene	0.87170	0.87171 <sup>c</sup>	415.98	417.58 <sup>c</sup>	
4	Metaxylene	0.86008	0.86009 <sup>a</sup>	412.01	412.25 <sup>e</sup>	

Table No.1: Densities (ρ) at T = 298.15 K and boiling points T of pure components at P =101.3 kPa

<sup>a</sup> from reference [14]. <sup>c</sup> from reference [16] <sup>d</sup> from reference [17] <sup>e</sup> from reference [18]

Table 10.2. I drameters of the Extended Antonie Equation										
S.No	Compound	A <sup>b</sup>	Bb	Cp	Db	Eb	F <sup>b</sup>	Gb	T1	T2
1	Nonane	102.44	-9030.40	0	0	-12.88	7.85E-6	2.00	219.66	594.60
2	Octane	89.17	-7900.20	0	0	-11.00	7.18E-6	2.00	216.38	568.70
3	Orthoxylene	83.49	-7955.00	0	0	-10.08	5.95E-6	2.0	247.98	630.30
4	Metaxylene	81.81	-7741.20	0	0	-9.86	6.07E-6	2.0	286.41	616.20

Table No.2: Parameters of the Extended Antoine Equation<sup>a</sup>

<sup>a</sup> Taken from Aspen property databank

<sup>b</sup> Extended Antoine equation:  $\ln(P^S) A_1 \underline{B_2} D_4T E_5 \ln T F_6 T C_7$  for

$$T_1 < T < T_2$$
, where  $P^S$  is in kPa and T in K.

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S.No	<i>T</i> /K	$X_1$		Y1	<i>T/</i> K		$\mathbf{X}_{1}$	Y <sub>1</sub>	
Nonane (A) + Octane (B)									
1	423.54	0	0		406.70		0.6192	0.6982	
2	420.72	0.1239		0.1241		404.68	0.7062	0.7694	
3	416.18	0.1265		0.1777	402.36		0.8051	0.8562	
4	409.92	0.2008		0.2721		399.94	0.9112	0.9381	
5	403.49	0.3058		0.3903		398.83	0.9622	0.9796	
6	398.64	0.4029		0.4854		398.32	1	1	
7	394.55	0.5113		0.5999					
Octane (A) + orthoxylene (B)									
8	398.32	0		0	407.20		0.6358	0.5219	
9	398.63	0.0553		0.0440		408.82	0.7175	0.6164	
10	399.33	0.1145		0.0969	411.14		0.8311	0.7309	
11	400.64	0.2071		0.1751		413.86	0.9183	0.8665	
12	402.36	0.3368	0.3368			414.17	0.9271	0.9984	
13	403.97	0.4346		0.3532		415.98	1	1	
14	405.59	0.5364	0.4431						
			C	Octane (A) + m	etaxyl	ene (B)			
15	398.32	0	0		412.35		0.6196	0.5348	
16	398.63	0.0552		0.0495		404.28	0.7114	0.6335	
17	399.13	0.1207		0.1101		405.59	0.8192	0.7578	
18	399.94	0.2165		0.1925	407.40		0.8853	0.8853	
19	401.05	0.3329		0.2897	409.52		0.9316	0.9991	
20	402.16	0.4291		0.3754	410.04		1	1	
21	403.27	0.5275		0.4601	411.99				
Table No.4: The NRTL and the UNIQUAC correlated parameters at 101.3 kPa for the systems studied									
S.No	System	Мо	del	Parameter/I	K	Parameter/K	RMSD T <sup>a</sup> /K	RMSD P <sup>a</sup> /kPa	
		NRT	ı b,c	g 12/R		3466.70	0.63	0.005	
2	Nonane + octane		1	g 21/R		403.05			
		UNIQ	UAC <sup>b</sup>	<i>u</i> 12/R		-15000	0.18	0.006	
		NDT	, b,c	<i>u</i> 12/R		449.62	0.63	0.008	
2	Octane + orthoxyler	ie INKI	L	g 12/R		-280.83	0100		
-			uncb	g 21/R		-3729.26	0.70	0.007	
		UNIQ	UNIQUAC			421.22	0.70		
		NDT	t b,c	<i>u</i> 12/R		-15000	0.58	0.006	
3	Octane + metavyler	INKI	L	<i>g</i> 12/R		-466.69	0.00	0.000	
5		UNIO	UAC <sup>b</sup>	<i>u</i> 12/R		430.73	0.83	0.005	
						-15000	0.03	0.005	

Table No.3: Experimental T, x<sub>1</sub> and y<sub>1</sub> results for the systems of nonane (A) with octane (B) and octane (A) orthoxylene (B) and metaxylene (B) at 101.3 kPa

<sup>a</sup> RMSD  $\Delta M = \sqrt{\frac{1}{np} \sum \sum_{k=1}^{np} (M_k^{calc} - M_k^{exp})^2}$ , where  $n_p$  is the number of data points and M represents T, P and  $x_1$ 

*u* 12/R

<sup>b</sup> NRTL model:  $T_{ij} = \Delta g_{ij}/RT$ ; UNIQUAC model:  $\ln T_{ij} = \Delta u_{12}/RT$ 

<sup>c</sup>The value of  $\alpha$  was fixed as 0.3 for each binary system

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Figure No.1: Plot of experimental boiling point temperatures at 101.3 kPa against mole fraction of nonane (1) and octane (2) (•), -, calculated liquid, vapour composition of the NRTL model., --- calculated liquid, vapour composition of the UNIQUAC model



Figure No.2: Plot of experimental boiling point temperatures at 101.3 kPa against mole fraction of octane (1) and orthoxylene (2) (•), -, calculated liquid, vapour composition of the NRTL model., --- calculated liquid, vapour composition of the UNIQUAC model

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Figure No.3: Plot of experimental boiling point temperatures at 101.3 kPa against mole fraction of octane (1) and metaxylene (2) (•), -, calculated liquid, vapour composition of the NRTL model., --- calculated liquid, vapour composition of the UNIQUAC model

#### CONCLUSION

Isobaric VLE results have been determined experimentally for binary mixtures composed of nonane with octane and octane with orthoxylene and metaxylene at 101.3 kPa over the entire range of compositions. The NRTL and the UNIQUAC models are capable of accurately correlating the VLE results of the systems investigated. The reported experimental results are satisfactorily correlated with these two models. The results reveal that all the systems studied exhibit non-ideal behaviour.

## ACKNOWLEDGEMENT

Financial support from the National Science Council (N.S.C), Taiwan, through Grant No. NSC 97-2811-E-011-003 is gratefully acknowledged.

## **CONFLICT OF INTEREST**

We declare that we have no conflict of interest.

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